

caeleste



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High Dynamic Range the pixel standpoint

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Examples of dynamic range scenes, extreme contrast scenes and what we would like to see in them
2. Dynamic range and S/N definitions ✓
There is not a single definition for S, N, and even less for DR. We base the definitions on “noise equivalent contrast” (NEC)
3. Non-linear response ✓
As a way to capture the highest possible dynamic range scenes. Derive which non-linear laws are optimal.



1. Why do we need a wide dynamic range?

Wide dynamic range scenes
Extreme contrast scenes



Why do we need a wide dynamic range?

- To catch highlights
- To allow us to be lazy and not adjust camera speed to the scene
- To discriminate objects in any part (dark/bright) of the scene

- Natural scenes
- Extreme contrast scenes





Highlight

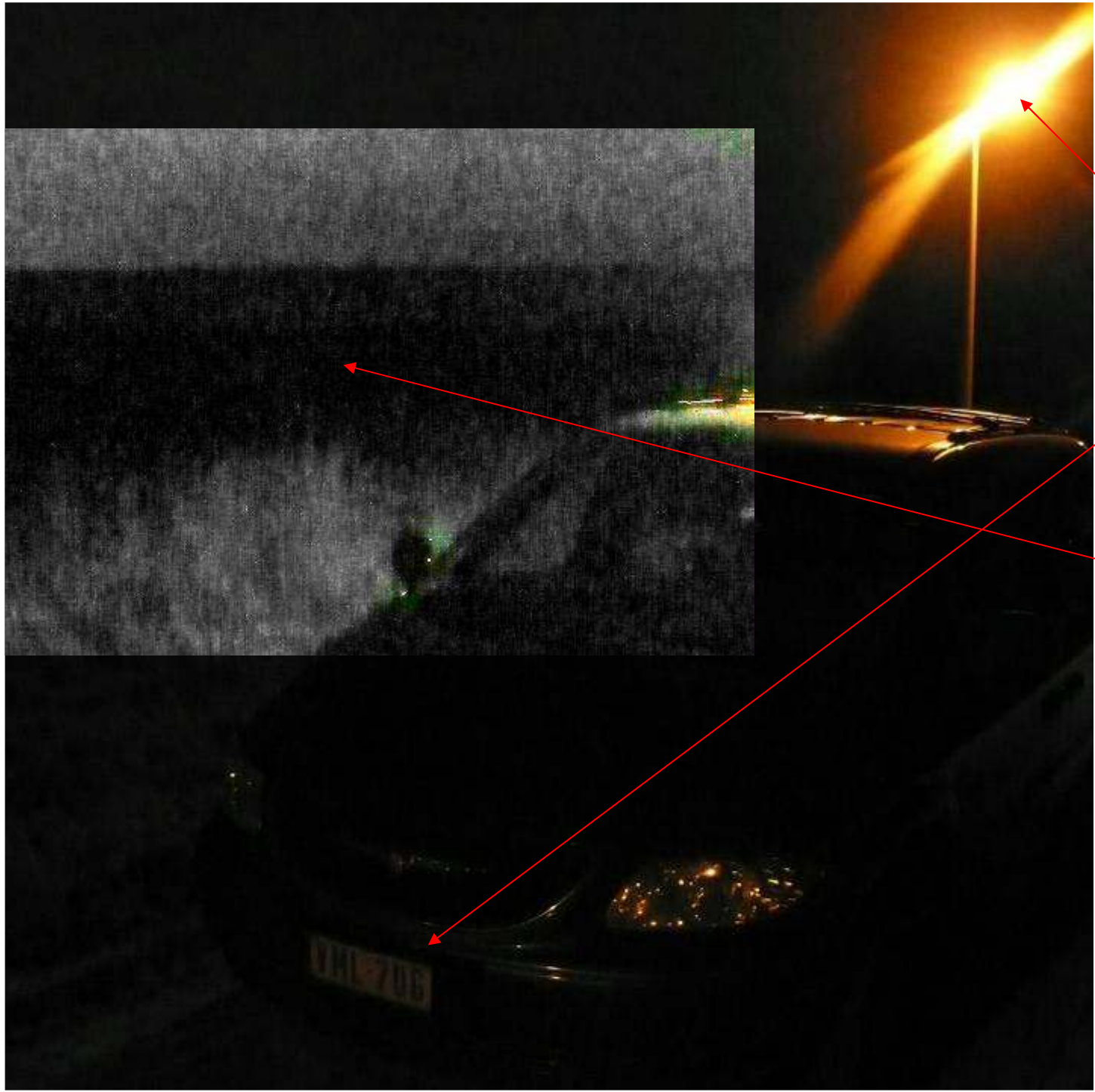
Hidden in Shadow

Retro-reflection

Dark objects

Deep dark space





High lights

Dark object
With some
contrast

Deep dark
background





Highlight
partly overexposed

In the shadow of a
shadowed scene





Deep shadow
No recovery

Heavy
overexposure
No recovery



100 dB scene

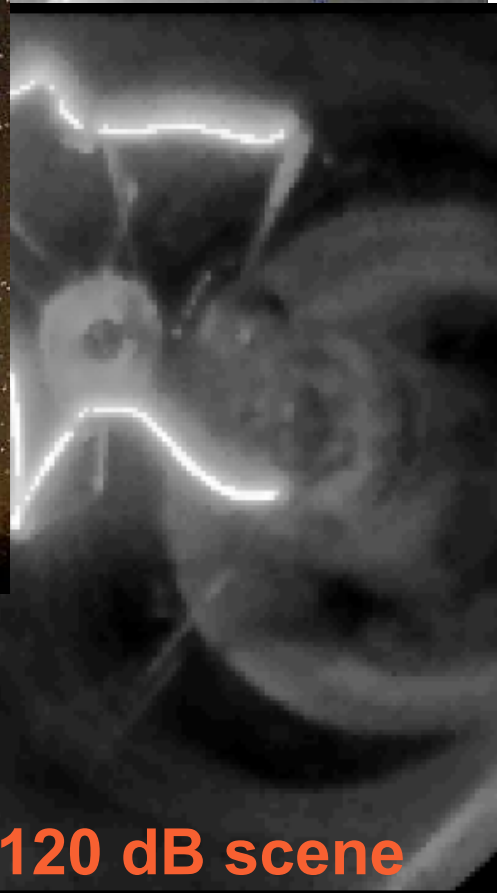


(courtesy Cypress Semiconductor)
From: B. Dierickx, J. Bogaerts, "STAR250
Radiation-tolerant APS for star tracker
applications", CNES atelier, Toulouse, June 3-4,
2002

140 dB scene



??? dB scene



100 dB scene

(Courtesy IMS Stuttgart) From: J.
Burghartz *, H. Graf, C. Harendt, W.
Klingler, H. Richter, M. Strobel, "HDR
CMOS Imagers and Their Applications"

120 dB scene



... and while grabbing a wide dynamic range scene...

Don't throw away the "sensitivity"

BTW what does sensitivity mean:

- High conversion ratio of light power to voltage?
- To see a faint signal in a limited exposure time?
- To see a faint signal in an unlimited exposure time?
- The ratio of the signal and the uncertainty thereof?



2. dynamic range definitions



Dynamic Range definition?

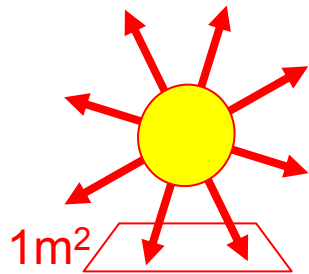
DR_{wikipedia}

Wikipedia: “Dynamic range is a term used frequently in numerous fields to describe the ratio between the smallest and largest possible values of a changeable quantity, such as in sound and light.”

Applies to the scene, not to the sensor

- our “changeable quantity” is “P”, “light” [W, W/m², photons, lux...]
- “signal”, “S”, is the measurement result [V, ADC bits...]

prior definitions

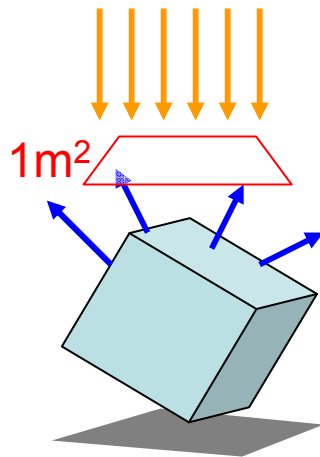


lamp
surface
(emittance)

Units:

W
Photons/s
Lumen
Candela

W/m^2
 $Photons/s \cdot m^2$
 $Lumen/m^2 = lux$



illuminant
(illuminance)

object reflection
(emittance)

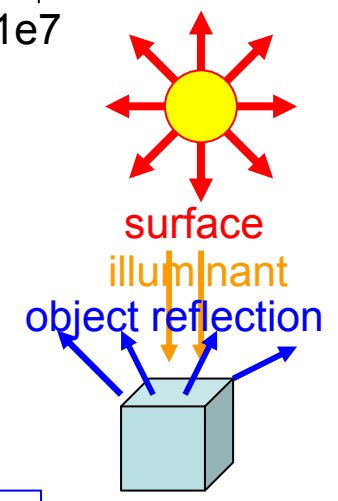
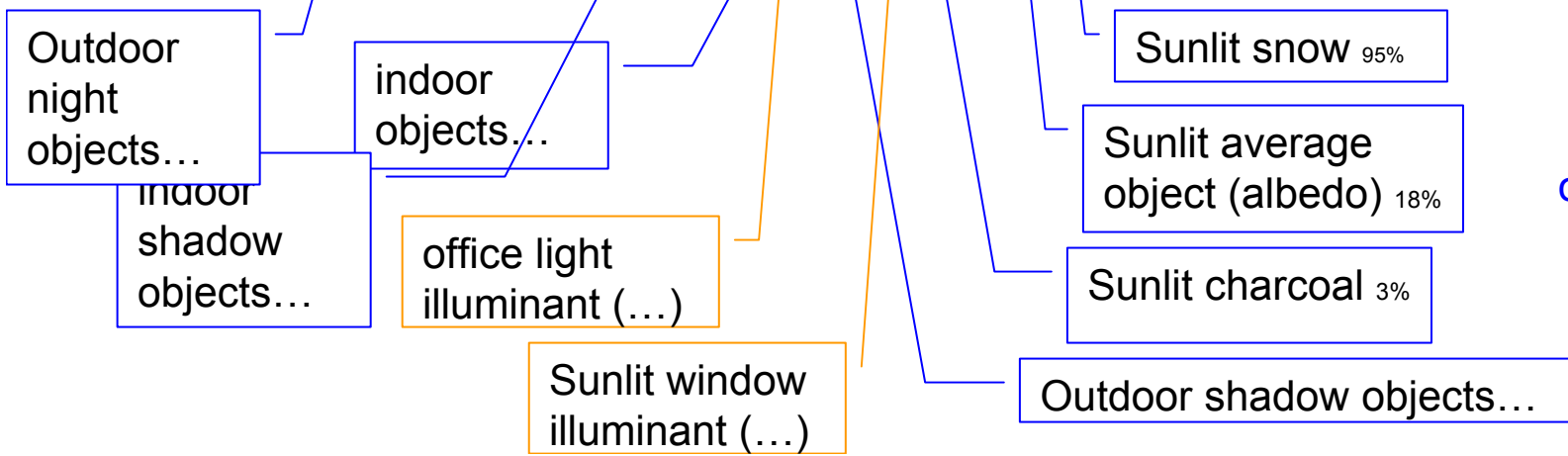
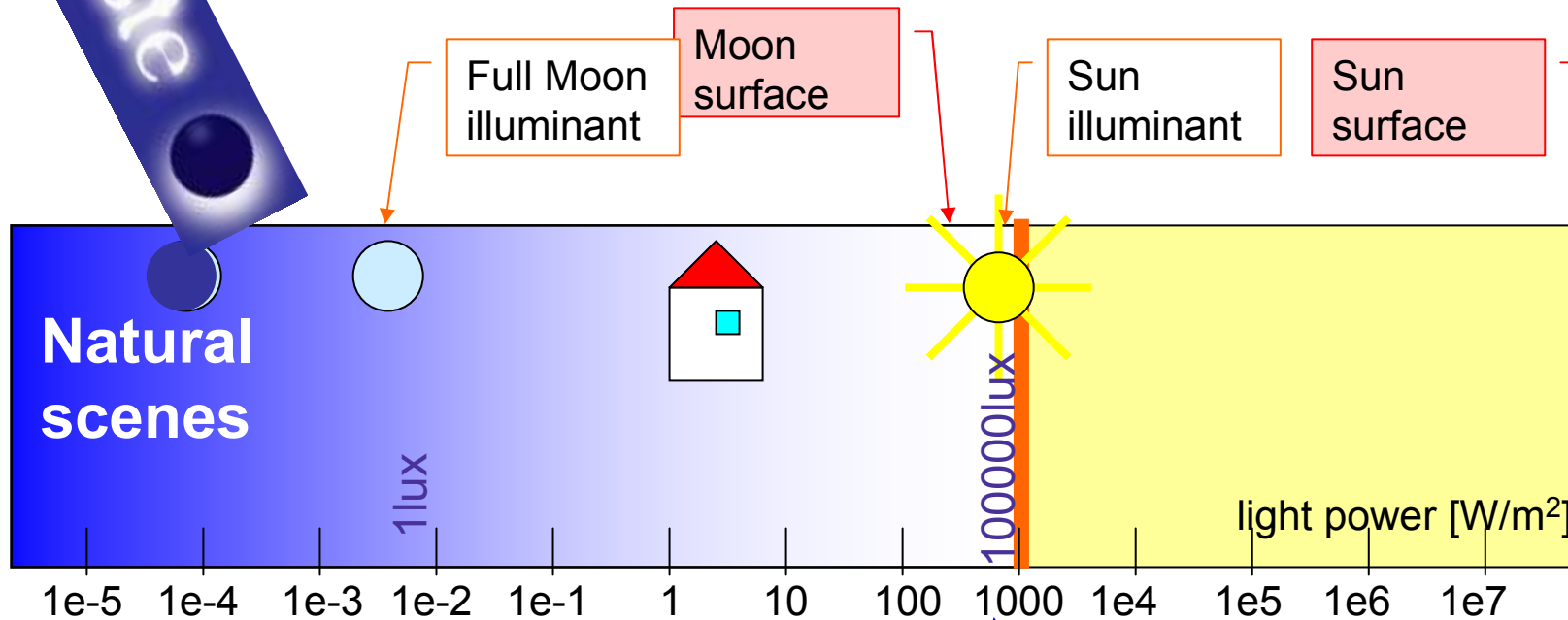
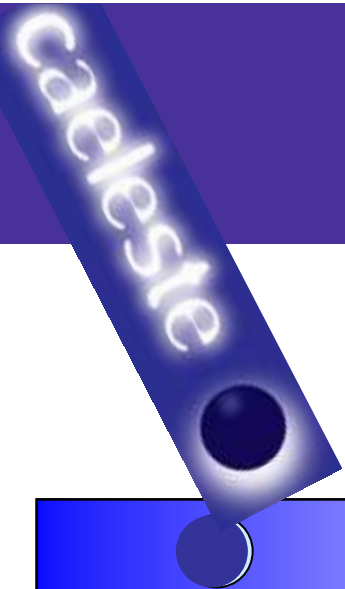
W/m^2
 $Photons/s \cdot m^2$
 $Lumen/m^2 = lux$

For white light
Between 400-700nm
 $1W \approx 150 \dots 250 \text{ Lumen}$

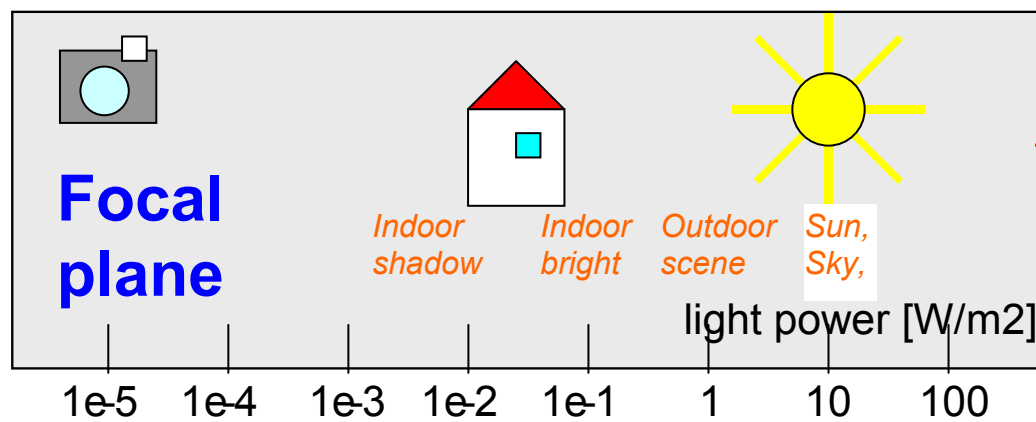
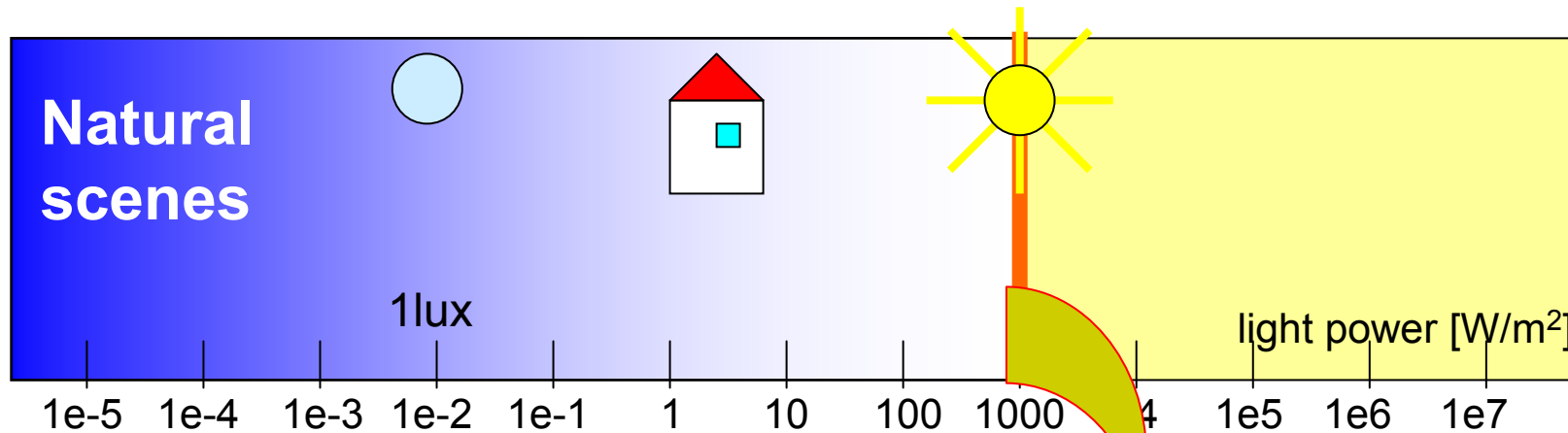
For white light
Between 400-700nm
 $1lux \cdot \mu m^2 \approx 4000 \text{ photons/s}$
 $1lumen \approx 4E15 \text{ photons/s}$
 $1W \approx 8e17 \text{ photons/s}$



Natural scenes

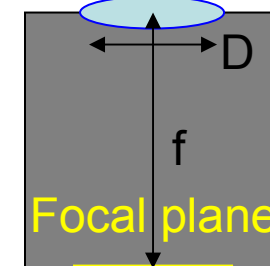


From scene to focal plane



optical attenuation

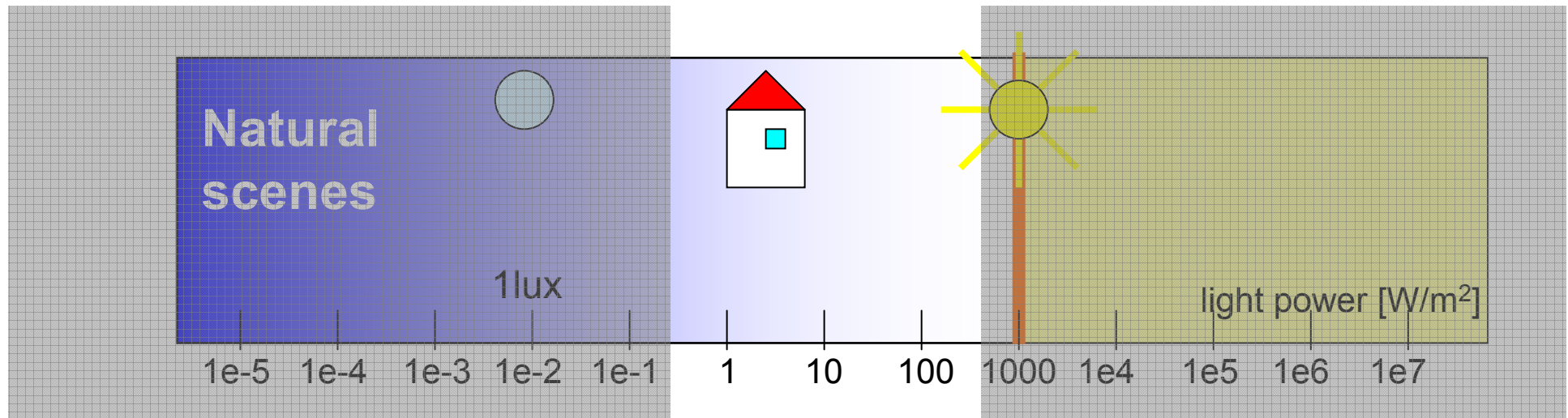
divide by $4F^2$
scene



$$F = f/D$$



With a linear response sensor



Linear response sensor:

S/N or SNR = Dynamic Range?

- typical: Between 1000: 1 = 60 dB
 - extreme high end: 10000:1 = 80 dB
- Dynamic range in sunlit scene: > 100 dB

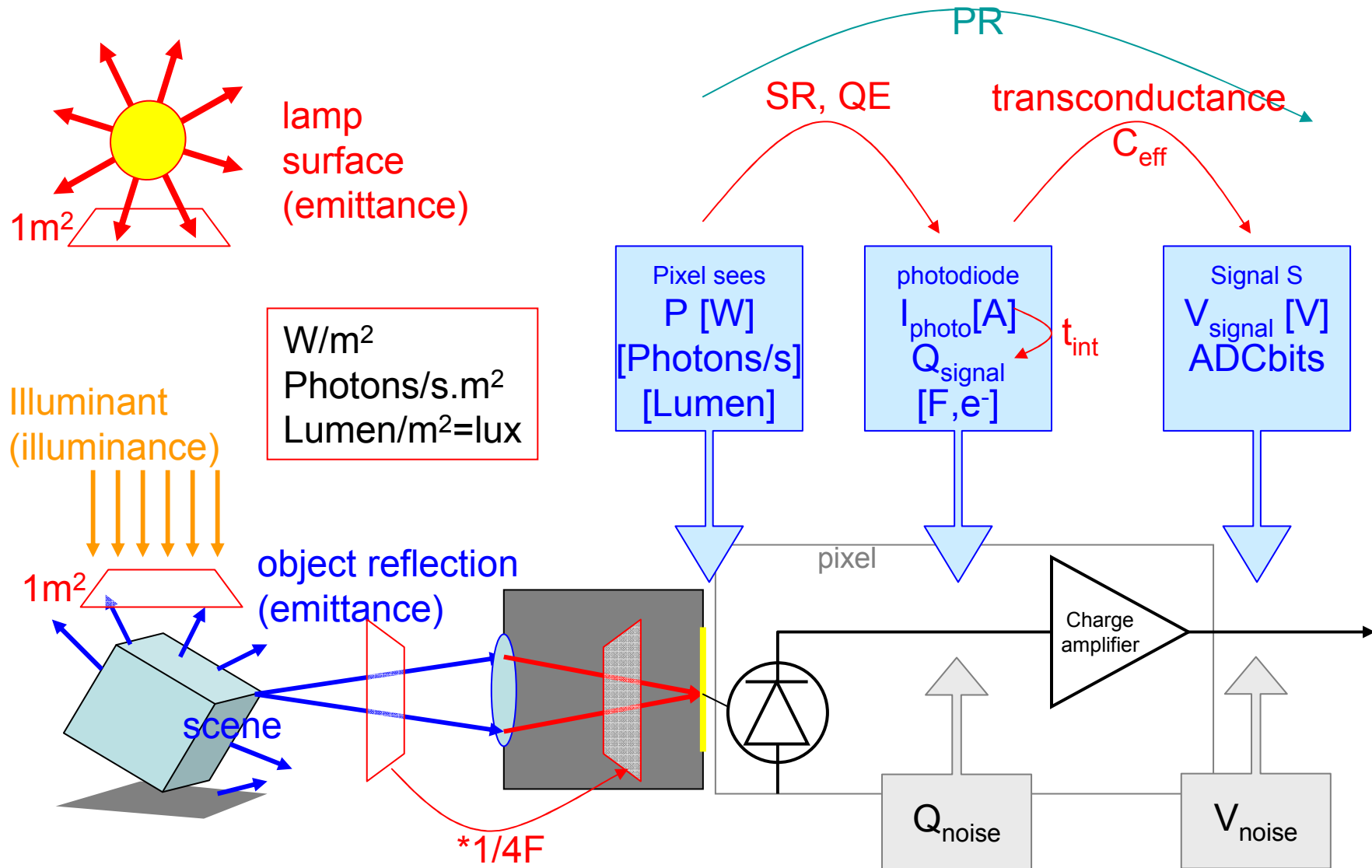
$$S \approx 1V, N \approx 1mV_{RMS}$$
$$S \approx 2V, N \approx 200\mu V_{RMS}$$

dynamic range definition, attempt 1

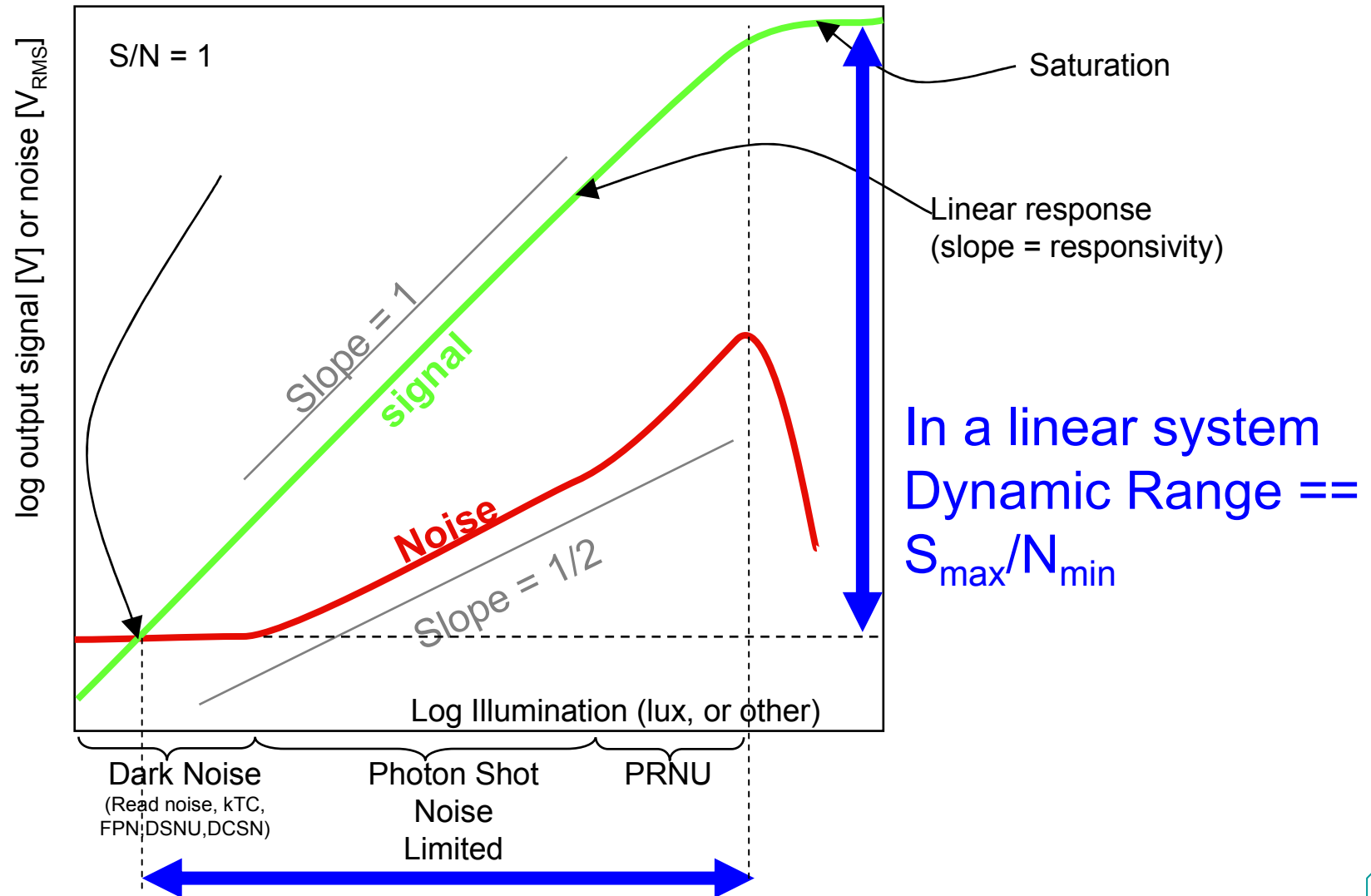
"DR is in light power domain what S_{max}/N_{min} is in voltage (signal) domain"



further definitions



DR = S/N ?



Maybe there are S/N definitions suitable for non-linear systems?

- Signal, S , V_{signal} [V]
 - The maximum signal: $S_{\text{max}}, V_{\text{max}} - V_{\text{dark}}$
 - At the working point, referred to Dark: $V - V_{\text{Dark}}$
 - Linearized around working point
 - Take into account $\partial V / \partial \text{illumination}$ or PR?
- Noise, N , V_{noise} [V_{RMS}]
 - At dark: N_{min}
 - Where $S/N = 1$
 - At the working point



What is part of N?

- Spatial noises
 - Fixed Pattern Noise
 - Temperature dependent: Dark signal non-uniformity (DSNU)
 - Signal dependent: Photo response non-uniformity (PRNU)
- Temporal noises
 - kTC, EMI, thermal and 1/f device noise, ...
 - Temperature dependent: Dark current shot noise (DCSN)
 - Signal dependent: Photon Shot Noise (PSN)

Issue: some of these can be / are calibrated

→Maximal noise: all of these

→Minimal noise: only PSN and DCSN



Noise breakdown

in 6 orthogonal categories

	Temporal noise (variation of the signal of one pixel over time)	Spatial noise (variation signals of pixels within a frame, steady over time)
Noise that is invariant for temperature, integration time and illumination level	Temporal noise <ul style="list-style-type: none"> •kTC noise, reset noise •other pixel and circuit noise •EMI (random EMI, Row noise, Interference...) •ADC noise 	Fixed pattern noise <ul style="list-style-type: none"> •Random FPN •Column/Row FPN •Other cosmetic flaws •EMI fixed interference patterns
Noise that depends on temperature and integration time	DCSN (dark current shot noise)	DSNU (Dark signal non-uniformity)
Noise that depends on the illumination level or signal level	PSN (photon shot noise)	Photo response non-uniformity <ul style="list-style-type: none"> •Random PRNU •Column PRNU •Other cosmetic flaws •Color PRNU

Dynamic Range definition?

DR_{wikipedia}

- *Wikipedia*: “Dynamic range is a term used frequently in numerous fields to describe the ratio between the smallest and largest possible values of a changeable quantity, such as in sound and light.”

Applies to the scene, not to the sensor

The sensor should be able to catch that range

What does that mean?



DR, attempt 2

Generalized dynamic range
definition, attempt 2

DR_{SNR1} = "ratio between
highest and lowest light
intensity for which S/N is
greater than or equal to 1".



Dynamic Range definitions

Further attempts for definition

- The range of light intensity levels that can be captured by the image sensor within a single frame
- The range of illumination levels on a similar object within the same frame, for which the object is recognizable (=decent contrast, after image processing)
- The range of intensities that can be captured, for which the SNR has at least a certain value
- The range of intensities that can be captured for which the Noise Equivalent Contrast (NEC) has at least a certain value

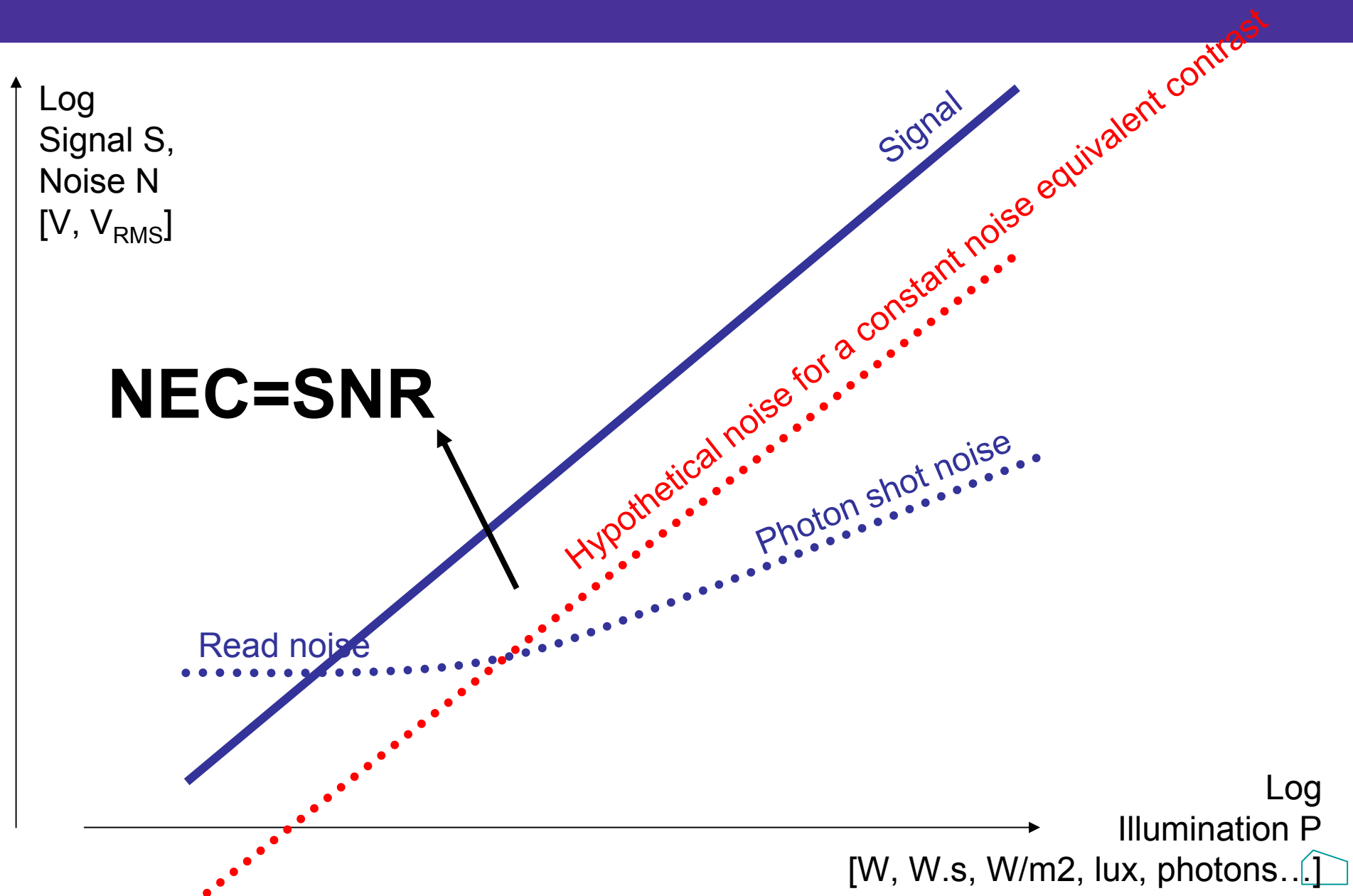


Ratios between the measured quantity and the uncertainty on that measurement

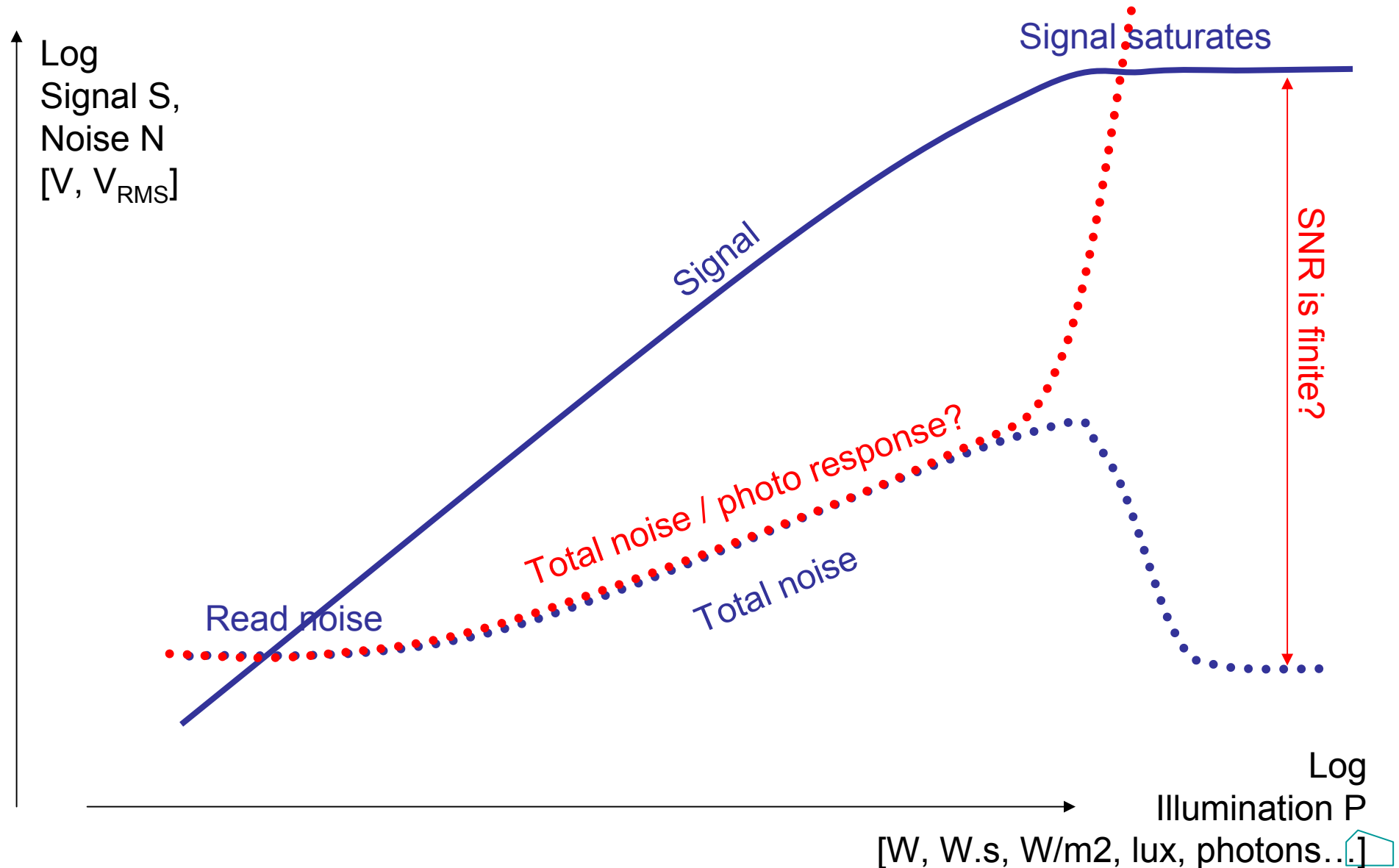
definition	Symbol	Unit	How to obtain
Signal to Noise Ratio	S/N_{\max} SNR_{\max}	1	sensor signal voltage range / sensor signal noise in the dark
Differential or small-signal signal to noise ratio	dS/dN $dSNR$	1	signal voltage / signal noise at that same signal level
Noise equivalent contrast ratio	NEC	1	The ability to discriminate between nearby grey levels $=1/(dSNR)*PR$ (where PR =photo response)
Dynamic range	DR_{\max}	1	Saturation <i>intensity</i> divided by noise equivalent <i>intensity</i> In a linear system this is the same as SNR_{\max}
Generalized dynamic range	DR_{SNR1}	1	the ratio between upper and lower <i>intensities</i> for which $dSNR \geq [\text{value}]$
Generalized dynamic range	DR_{NEC10}	1	the ratio between upper and lower <i>intensities</i> for which $NEC \geq [\text{value}]$
Linear dynamic range	LDR_x	1	DR_x with largest intensity for which $d\text{Volt}/d\text{Intensity}$ is linear
ADC bits		1	Number of (useful) bits in the sensor's digital output
bits		1	Number of bits after image processing

Disclaimer: these suffixes are a clarification for this course. They are not used in practice.

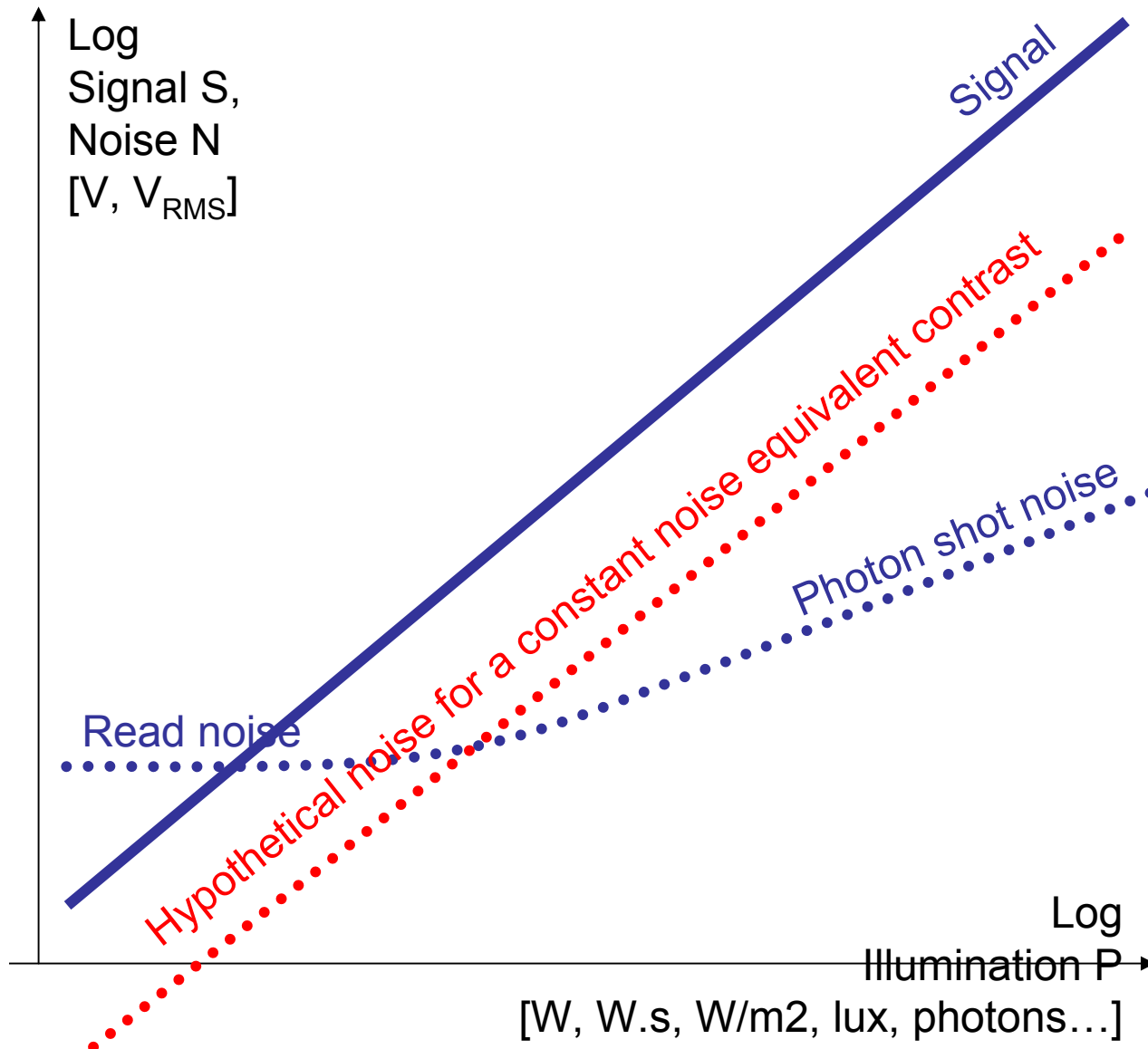
Constant N.E.Contrast - linear



In a non-linear system $SNR \neq NEC$



Noise Equivalent Contrast - **general**



$$NEC = \frac{P}{NEP}$$

$$NEP = \frac{\bar{N}}{\text{Photoresponse}} = \frac{\bar{N}}{\left(\frac{\partial S}{\partial P}\right)}$$

$$NEC = \frac{P}{NEP} = \frac{P \cdot \frac{\partial S}{\partial P}}{N}$$



Noise Equivalent Contrast – non-linear

$$V_{\text{signal}} = S$$

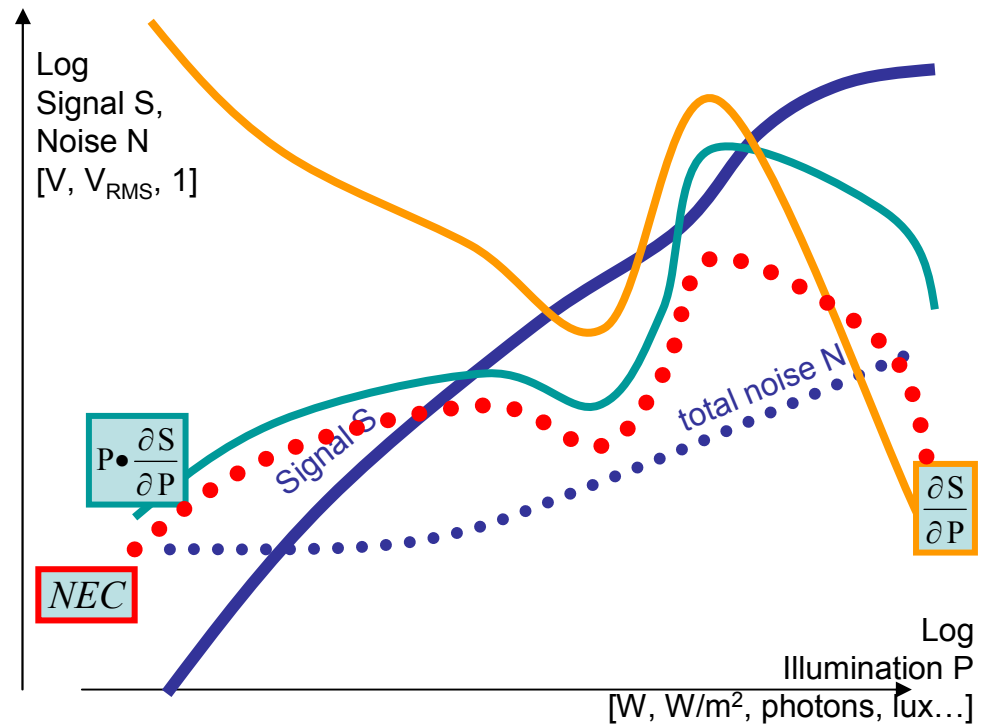
$$V_{\text{noise}} = N$$

$$NEC = \frac{P}{NEP}$$

$$NEP = \frac{N}{\text{Photoresponse}} = \frac{N}{\left(\frac{\partial S}{\partial P}\right)}$$

$$NEC = \frac{P}{NEP} = \frac{P \cdot \frac{\partial S}{\partial P}}{N}$$

(In a linear system $NEC == S/N$)



Relation between NEC and Wide DR

- Goal: reach a constant or minimal NEC over the largest possible [dynamic range]_{wikipedia definition}
- Unproven underlying hypothesis: the largest range is obtained when NEC is just large enough, i.e. constant

$$NEC = \frac{P}{NEP} = \frac{P \cdot \frac{\partial S}{\partial P}}{N} = \text{constant}$$



In search for a constant NEC

- Exercise of thought:

- Obtain the constant NEC by exploiting non-linear response

- Increase DR by sacrificing NEC where it is sufficient

- Non-linear response is obtained by

- A non-linear transconductance, gain or $C_{\text{effective}}$
- A non-linear integration time t_{int}

$$V_{\text{signal}} = \frac{t_{\text{int}} \cdot I_{\text{photo}}}{C_{\text{eff}}}$$

- In the presence of noise of following kinds

- A fixed amount in charge or light (as kTC...)
- A fixed amount in voltage (other read noise, circuit noise)
- Proportional to the $\sqrt{\text{power}}$ (photon shot noise, PSN)
- Proportional to the $\sqrt{\text{integration time}}$ (dark current shot noise, DCSN)
- Proportional to the power (photo response non-uniformity, PRNU)
- Proportional to the integration time (Dark signal non-uniformity, DSNU)



Is ISO a potential measure for dynamic range?

method	Formula	Border conditions
MMS Bristol's	$ISO = 0.2 [W.s/m^2] / (t_{int}[s] * P[W/m^2])$	White light, P is average of scene, 50% of saturation
Basler's	100 ISO corresponds to 0.1 Lux*sec	Where the average P is at 18% of a linear grey scale
Michael Kriss'	ISO Speed = 0.8/H	at a signal-to-noise ratio of 30
Interpreting ISO12232	ISO == (1.92 lx.s)/Lf.t Lf [lx] = focal plane luminance	at 18%...50% of saturation - <i>the level of saturation itself is a parameter that one may change</i>
Kodak's "saturation based" ISO	$ISO = (15.4 * f^2) / (L_s * t)$	Ls[lx] = scene luminance 18/106 saturation (18/170 for professional photography)
Kodak's "noise based" ISO	ISO = 10 / H H = exposure in [lx.s]	SNR is either 40 (excellent image) or 10 (acceptable image), all noises included

Does not account for color information	Does not account for image processing
Does not account for effect of resolution on subjective perception	Does not account for dynamic range



3. non-linearity

non-linear response as a way to increase the sensor's capability to capture a wide dynamic range scene

non-linear response as a way to exploit the fact that the noise level depends on the scene contents



“dynamic range > 80 dB cannot be reached with a linear response sensor” – so what?

$$V_{signal} = \frac{t_{int} \cdot I_{photo}}{C_{eff}}$$

$$V_{signal} = \frac{Q_{signal}}{C_{eff}}$$

$$V_{noise} = \frac{Q_{noise}}{C_{eff}}$$

Modulation of the integration time

- Multiple slope response (piece-wise linear slopes)
- Non Destructive Readout

Modulation of the time constant

- Logarithmic response
- Lin-log

Modulation of the integration capacitance

- CCD with two wells
- Overflow MOSFET capacitors
- Adding multiple shorter integration periods
- Smart reset pixels



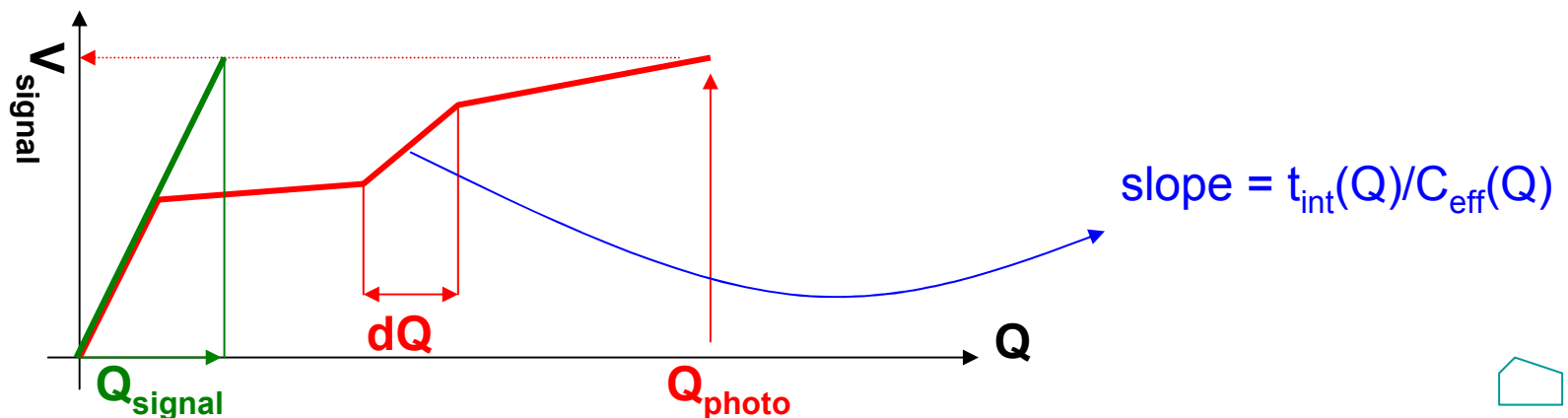
Non-linear version of $V_{\text{signal}}(Q)$

$$V_{\text{signal}} = \frac{t_{\text{int}} \cdot I_{\text{photo}}}{C_{\text{eff}}} \quad (\text{linear})$$

$$V_{\text{signal}} = \sum \frac{t_{\text{int}} \cdot I_{\text{photo}}}{C_{\text{eff}}} = \frac{Q_{\text{photo}}}{t_{\text{int max}}} \cdot \sum \frac{t_{\text{int}}(Q)}{C_{\text{eff}}(Q)}$$

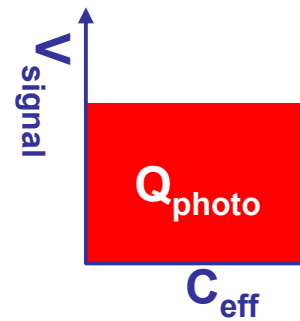
$$V_{\text{signal}} = \frac{1}{t_{\text{int max}}} \cdot \int_0^{Q_{\text{photo}}} \frac{t_{\text{int}}(Q)}{C_{\text{eff}}(Q)} dQ$$

- We assume that the total photo charge is cut in pieces
- Each piece may have a different integration time or integration capacitor.
- Think on a charge accumulation axis, not on a time axis

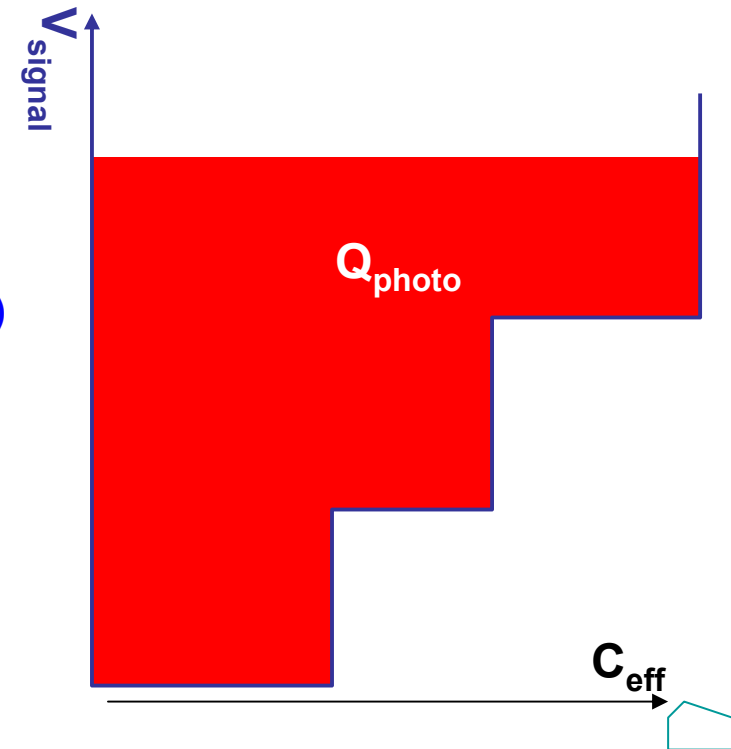
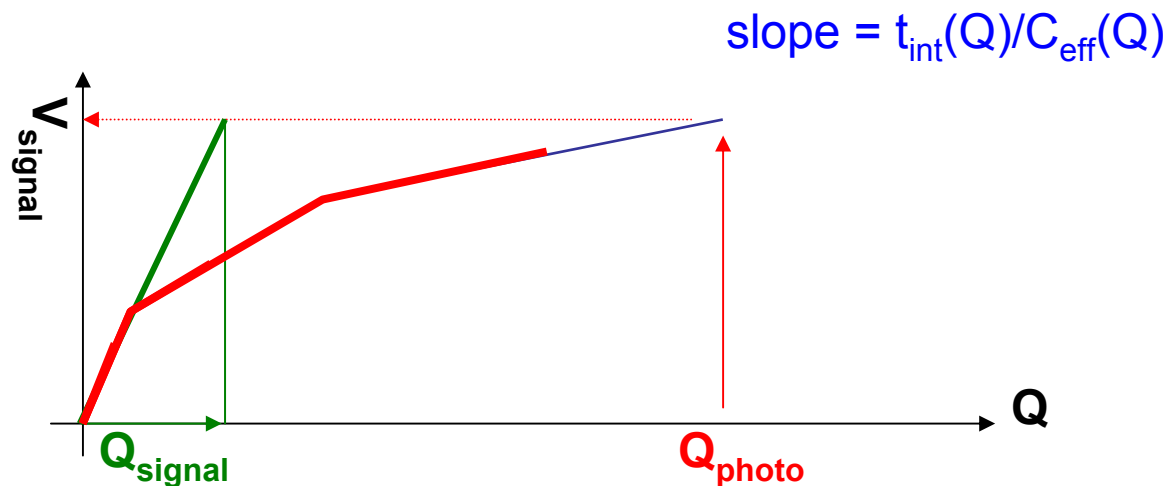


Non-linear version of $V_{\text{signal}}(Q)$ (2)

$$V_{\text{signal}} = \frac{t_{\text{int}} \cdot I_{\text{photo}}}{C_{\text{eff}}} \quad (\text{linear})$$



$$V_{\text{signal}} = \sum \frac{t_{\text{int}} \cdot I_{\text{photo}}}{C_{\text{eff}}} = \frac{Q_{\text{photo}}}{t_{\text{int max}}} \cdot \sum \frac{t_{\text{int}}(Q)}{C_{\text{eff}}(Q)}$$



Is non-linearity mandatory?

Non-linearity (non-linear response) is *not* essential.
(e.g. *Non-Destructive Readout* is a linear method)

It may be considered as a feature of the acquisition process, helping to catch the wide range of intensities in the image

It *may* do so by taking noise levels (NEC!) into account

In a post-processing step the non-linearity may be linearized



Formula for NEC in charge domain

$$NEC = \frac{P}{NEP} = \frac{P \cdot \frac{\partial S}{\partial P}}{N}$$

$P \sim Q_{photo}$ total photo charge during frame time

Q_{signal} charge integrated during t_{int}

$N \sim Q_{noise}$ uncertainty on Q_{signal}

$Q_{signal}/Q_{photo} = t_{int}/t_{intmax}$

$V_{signal} = S$

$V_{noise} = N$

$$\Rightarrow NEC = \frac{Q_{photo} \cdot \frac{\partial Q_{signal}}{\partial Q_{photo}}}{Q_{noise}}$$

$$\frac{\partial Q_{signal}}{\partial Q_{photo}} = \frac{\partial t_{int}}{\partial P} \cdot \frac{P}{t_{intmax}} = \frac{\partial t_{int}}{\partial Q_{photo}} \cdot \frac{Q_{photo}}{t_{intmax}}$$

$$\Rightarrow NEC = \frac{Q_{photo} \cdot \frac{\partial t_{int}}{\partial Q_{photo}} \cdot \frac{Q_{photo}}{t_{intmax}}}{Q_{noise}}$$

NEC does not depend on C_{eff} in charge domain 

Formula for NEC in voltage domain

$$NEC = \frac{P}{NEP} = \frac{P \cdot \frac{\partial S}{\partial P}}{N}$$

$$V_{signal} = \int \frac{t_{int} \cdot I_{photo}}{C_{eff}} = \int \frac{t_{int} \cdot P \cdot SR}{C_{eff}}$$

$$V_{signal} = S$$

$$V_{noise} = N$$

$SR = \text{Spectral Response [A/W]}$

$$\frac{\partial S}{\partial P} = SR \cdot \left(\frac{t_{int}}{C_{eff}} + \frac{\frac{\partial t_{int}}{\partial P} \cdot P}{C_{eff}} - \frac{t_{int} \cdot P \cdot \frac{\partial C_{eff}}{\partial P}}{C_{eff}^2} \right)$$

When one lets integration time depend on P or Q_{photo}

$$NEC = \frac{P}{N} \cdot \frac{\partial S}{\partial P} = \frac{SR \cdot \left(\frac{t_{int} \cdot P}{C_{eff}} + \frac{\frac{\partial t_{int}}{\partial P} \cdot P^2}{C_{eff}} - \frac{t_{int} \cdot P^2 \cdot \frac{\partial C_{eff}}{\partial P}}{C_{eff}^2} \right)}{N}$$

When one lets C_{eff} depend on P or Q_{photo}



Keep NEC constant... in the presence of a fixed noise charge

t_{int} varies

$$NEC = \frac{\frac{\partial t_{\text{int}}}{\partial Q_{\text{photo}}} \cdot \frac{Q_{\text{photo}}^2}{t_{\text{int max}}}}{Q_{\text{noise}}}$$

$Q_{\text{noise}} = \text{constant}$

$$\frac{\partial t_{\text{int}}}{\partial Q_{\text{photo}}} \sim \frac{1}{Q_{\text{photo}}^2}$$

$$t_{\text{int}}(Q_{\text{photo}}) \sim \frac{1}{Q_{\text{photo}}}$$

C_{eff} varies

$$NEC = \frac{Q_{\text{signal}}}{Q_{\text{noise}}} = \frac{Q_{\text{photo}}}{Q_{\text{noise}}}$$

No solution

i.e. there is no $C_{\text{eff}}(P)$ law that results in a constant NEC when noise a fixed charge. (This does not prohibit the use of C_{eff} modulation in general)



Keep NEC constant... in the presence of kTC noise

t_{int} varies

$$NEC = \frac{\frac{\partial t_{\text{int}}}{\partial Q_{\text{photo}}} \cdot \frac{Q_{\text{photo}}^2}{t_{\text{int max}}}}{Q_{\text{noise}}}$$

$Q_{\text{noise}} = \text{constant (!)}$

$$\frac{\partial t_{\text{int}}}{\partial Q_{\text{photo}}} \sim \frac{1}{Q_{\text{photo}}^2}$$

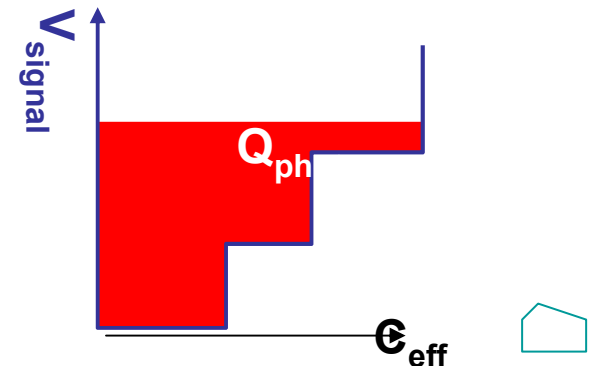
$$t_{\text{int}}(Q_{\text{photo}}) \sim \frac{1}{Q_{\text{photo}}}$$

C_{eff} varies

$$NEC = \frac{Q_{\text{photo}}}{Q_{\text{noise}}}$$

$$Q_{\text{noise}} = \sqrt{kTC_{\text{eff}}} \sim \sqrt{C_{\text{eff}}}$$

$$C_{\text{eff}} \sim Q_{\text{photo}}^2$$



Keep NEC constant... in the presence of photon shot noise

t_{int} varies

$$NEC = \frac{\frac{\partial t_{\text{int}}}{\partial Q_{\text{photo}}} \cdot \frac{Q_{\text{photo}}^2}{t_{\text{int max}}}}{Q_{\text{noise}}}$$

$$Q_{\text{noise}} \sim \sqrt{Q_{\text{signal}}} \sim \sqrt{Q_{\text{photo}} \cdot t_{\text{int}}}$$

$$\frac{\partial t_{\text{int}}}{\partial Q_{\text{photo}}} \sim \frac{\sqrt{Q_{\text{photo}}} \cdot \sqrt{t_{\text{int}}}}{Q_{\text{photo}}^2}$$

$$t_{\text{int}}(Q_{\text{photo}}) \sim \frac{1}{Q_{\text{photo}}}$$

C_{eff} varies

$$NEC = \frac{Q_{\text{photo}}}{Q_{\text{noise}}}$$

$$Q_{\text{noise}} \sim \sqrt{Q_{\text{photo}}}$$

No solution

i.e. there is no $C_{\text{eff}}(P)$ law that results in a constant NEC when noise is exclusively PSN. This does not prohibit the use of C_{eff} modulation in general



Keep NEC constant... when dominated by PRNU

t_{int} varies

$$NEC = \frac{\frac{\partial t_{\text{int}}}{\partial Q_{\text{photo}}} \cdot \frac{Q_{\text{photo}}^2}{t_{\text{int max}}}}{Q_{\text{noise}}}$$

$$Q_{\text{noise}} \sim Q_{\text{signal}} \sim Q_{\text{photo}} \cdot t_{\text{int}}$$

$$\frac{\partial t_{\text{int}}(Q)}{\partial Q_{\text{photo}}} \sim \frac{t_{\text{int}}(Q)}{Q_{\text{photo}}}$$

Always fulfilled

C_{eff} varies

$$NEC = \frac{Q_{\text{photo}}}{Q_{\text{noise}}}$$

$$PRNU = \frac{Q_{\text{noise}}}{Q_{\text{photo}}} = \text{constant}$$

Always fulfilled

i.e. for any relation $C_{\text{eff}}(P)$, NEC is constant for systems dominated by PRNU



Keep NEC constant in the presence of a fixed voltage noise

t_{int} varies

$$NEC = \frac{SR \cdot \left(\frac{\partial t_{\text{int}}}{\partial P} \cdot P^2 \right)}{N}$$

$$V_{\text{noise}} = \text{constant} \sim \frac{\partial t_{\text{int}}}{\partial P} \cdot P^2$$

$$\frac{\partial t_{\text{int}}}{\partial P} \sim \frac{1}{P^2}$$

$$t_{\text{int}}(P) \sim \frac{1}{P}$$

C_{eff} varies

$$NEC = \frac{SR \cdot \left(\frac{t_{\text{int}} \cdot P^2 \cdot \frac{-\partial C_{\text{eff}}}{\partial P}}{C_{\text{eff}}^2} \right)}{N}$$

$$V_{\text{noise}} = \text{constant} \sim \frac{P^2 \cdot \frac{\partial C_{\text{eff}}}{\partial P}}{C_{\text{eff}}^2}$$

$$\frac{\partial C_{\text{eff}}}{\partial P} \sim \frac{C_{\text{eff}}^2}{P^2}$$

$$C_{\text{eff}} \sim P$$



Keep NEC constant...

when dominated by dark current shot noise

t_{int} varies

$$NEC = \frac{\frac{\partial t_{\text{int}}}{\partial Q_{\text{photo}}} \cdot \frac{Q_{\text{photo}}^2}{t_{\text{int max}}}}{Q_{\text{noise}}}$$

$$Q_{\text{noise}} \sim \sqrt{t_{\text{int}}}$$

$$\frac{\partial t_{\text{int}}}{\partial Q_{\text{photo}}} \sim \frac{\sqrt{t_{\text{int}}}}{Q_{\text{photo}}^2}$$

$$t_{\text{int}}(Q_{\text{photo}}) \sim \frac{1}{Q_{\text{photo}}^2}$$

C_{eff} varies

$$NEC = \frac{Q_{\text{photo}}}{Q_{\text{noise}}}$$

$$Q_{\text{noise}} \sim \text{constant}$$

No solution



Keep NEC constant... when dominated by DSNU

t_{int} varies

$$NEC = \frac{\frac{\partial t_{\text{int}}}{\partial Q_{\text{photo}}} \cdot \frac{Q_{\text{photo}}^2}{t_{\text{int max}}}}{Q_{\text{noise}}}$$

$$Q_{\text{noise}} \sim t_{\text{int}}$$

$$\frac{\partial t_{\text{int}}}{\partial Q_{\text{photo}}} \sim \frac{t_{\text{int}}}{Q_{\text{photo}}^2}$$

No solution

C_{eff} varies

$$NEC = \frac{Q_{\text{photo}}}{Q_{\text{noise}}}$$

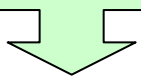
$$Q_{\text{noise}} \sim \text{constant}$$

No solution



Summary of “keep NEC constant”

Nature of noise



Noise sources that persist after calibration in high end imagers

t_{int} varies

C_{eff} varies

$$NEC = \frac{SR \cdot \left(\frac{\partial t_{int} \cdot P^2}{\partial P} \right)}{N \cdot C_{eff}}$$

$$NEC = \frac{SR \cdot \left(t_{int} \cdot P^2 \cdot \frac{-\partial C_{eff}}{\partial P} \right)}{N \cdot C_{eff}^2}$$

$$NEC = \frac{Q_{photo} \cdot \frac{\partial Q_{signal}}{\partial Q_{photo}}}{Q_{noise}}$$

$$NEC = \frac{Q_{photo}}{Q_{noise}}$$

Constant charge _{RMS}	kTC noise	$t_{int} \sim 1/Q$	$C_{eff} \sim Q^2$
Constant voltage _{RMS}	EMI, read noise, ADC...	$t_{int} \sim 1/Q$	$C_{eff} \sim Q$
$\sim \sqrt{\text{power}}$	PSN	$t_{int} \sim 1/Q$	No solution
$\sim \sqrt{t_{int}}$	DCSN	$t_{int} \sim 1/Q^2$	No solution
$\sim \text{power}$	PRNU	always	always
$\sim t_{int}$	DSNU	No solution	No solution



interpretation

One can define a $t_{\text{int}}(Q)$ or $C_{\text{eff}}(Q)$ law to obtain a constant and optimal NEC for most common noise signatures

The relations $t_{\text{int}} \sim 1/Q$ and $C_{\text{eff}} \sim Q$ found are essentially “logarithmic responses”

$$V_{\text{signal}} = \frac{1}{t_{\text{int max}}} \cdot \int_0^{Q_{\text{photo}}} \frac{t_{\text{int}}(Q)}{C_{\text{eff}}(Q)} dQ \sim \int_0^{Q_{\text{photo}}} \frac{1}{Q} dQ$$

$$V_{\text{signal}} \sim \log_n(Q_{\text{photo}}) + Cte$$

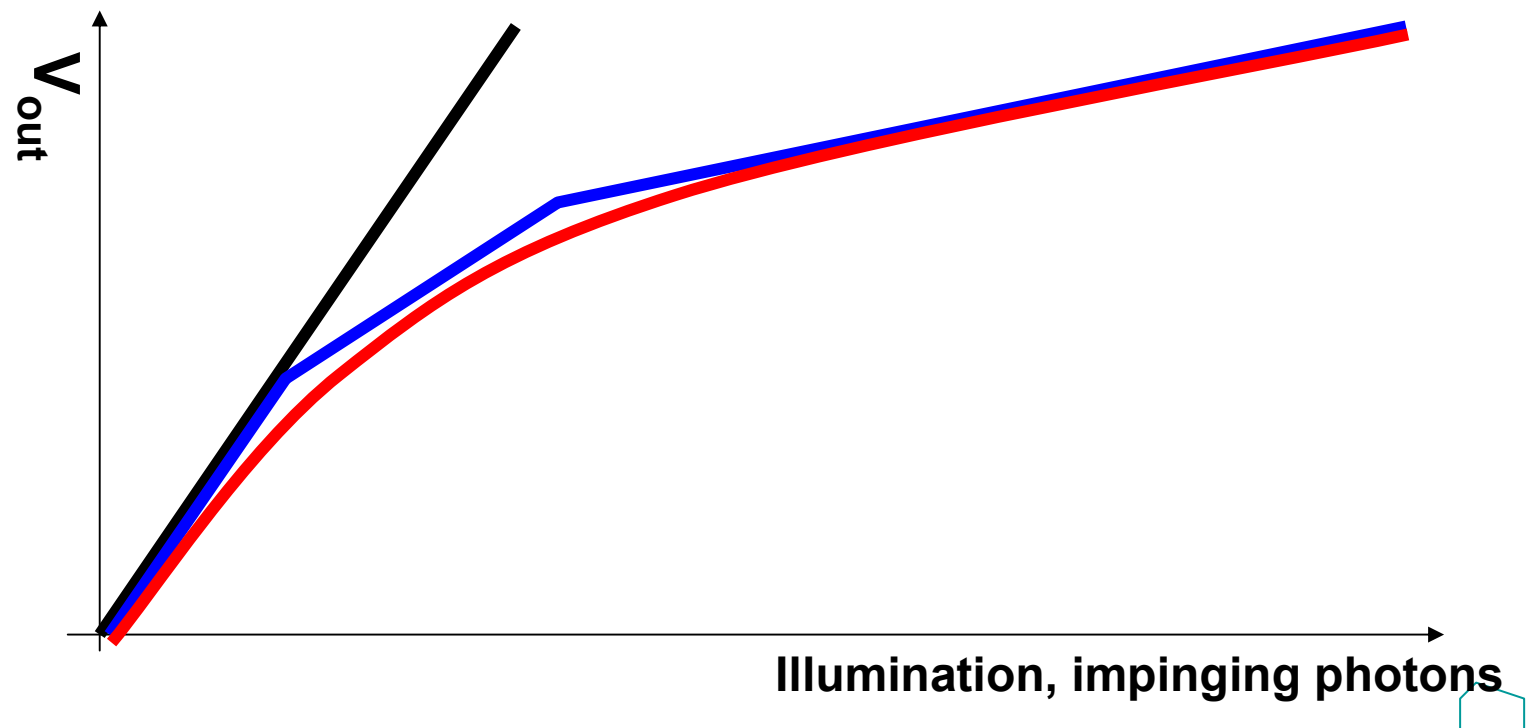
For $t_{\text{int}} \sim 1/P^2$ and $C_{\text{eff}} \sim P^2$:

$$V_{\text{signal}} \sim \int_0^{Q_{\text{photo}}} \frac{1}{Q^2} dQ$$

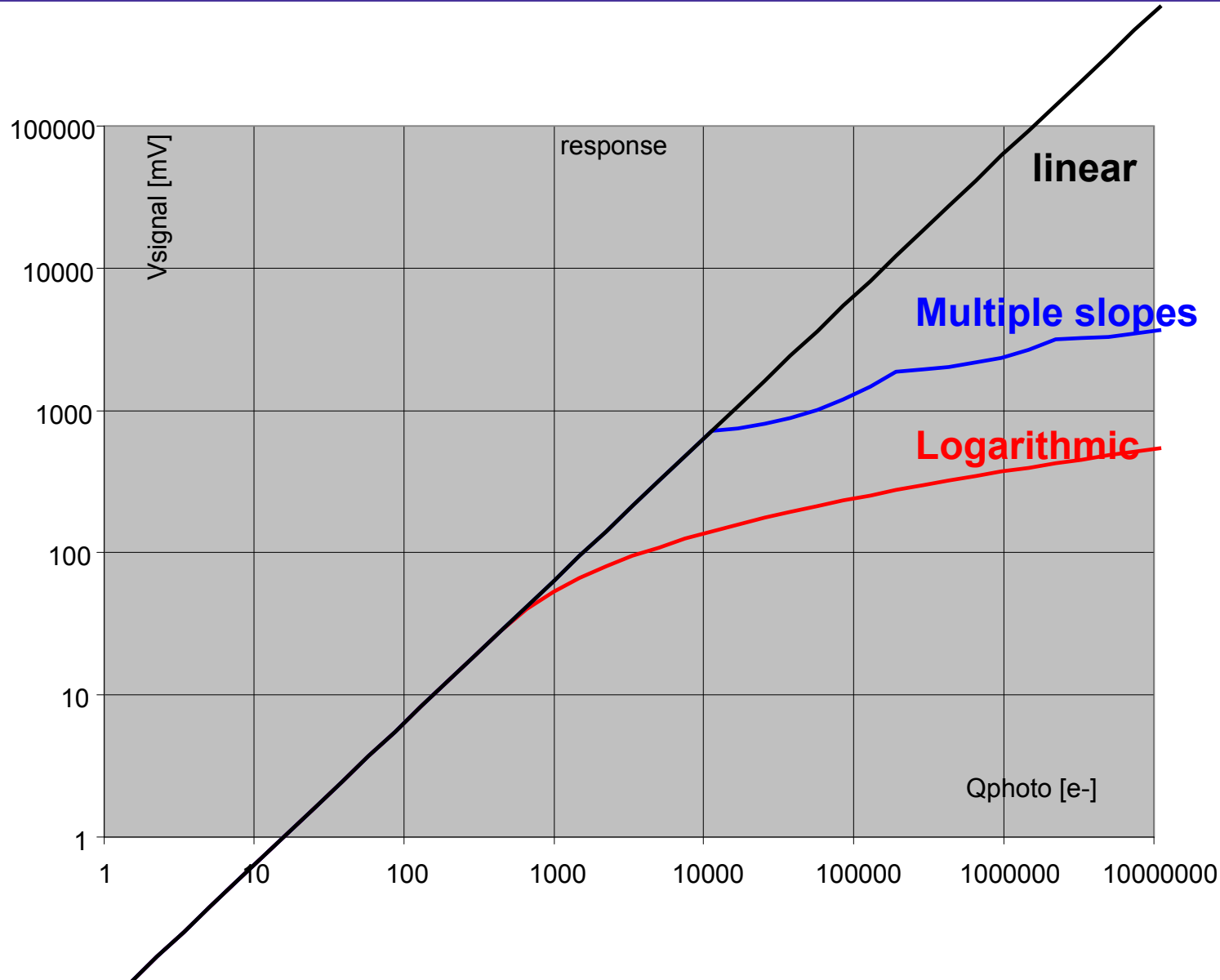
$$V_{\text{signal}} \sim \frac{1}{Q_{\text{photo}}} + Cte$$

illustration

- Linear response
- Logarithmic response for $NEC \approx 10$
- Approximation multiple slopes for $NEC \geq 10$



Result $NEC \geq 10$



Noise sources considered:

- PSN
- Read noise 1mV_{RMS}

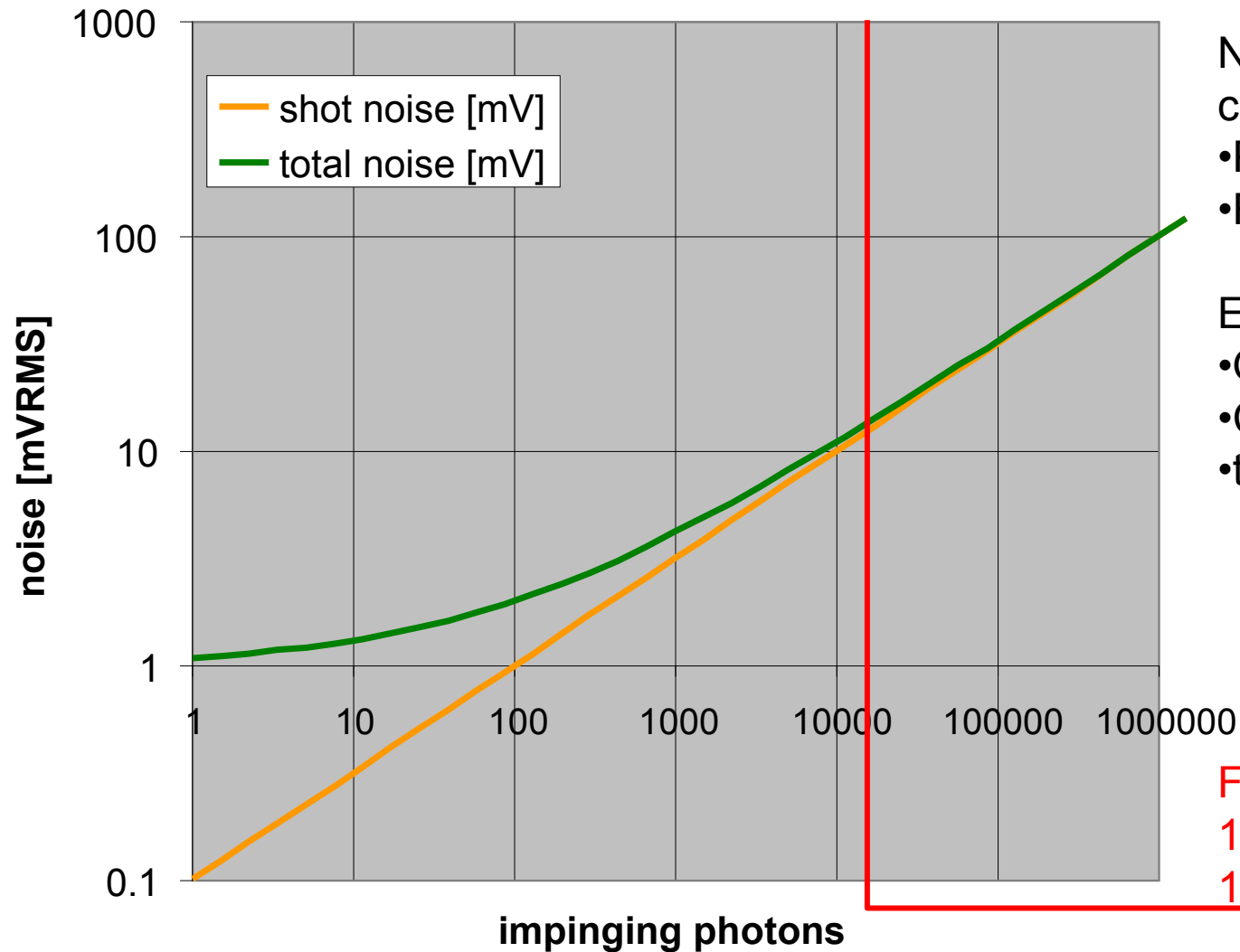
Essential pixels specs

- QE = 40%
- $C_{\text{eff}} = 1\text{fF}$
- t_{int} = not specified

Full well limit \approx
 $1\text{fF} * 1\text{V} \approx 6000\text{e}^-$
15000 photons



Linear response



Noise sources considered:

- PSN
- Read noise 1mV_{RMS}

Essential pixels specs

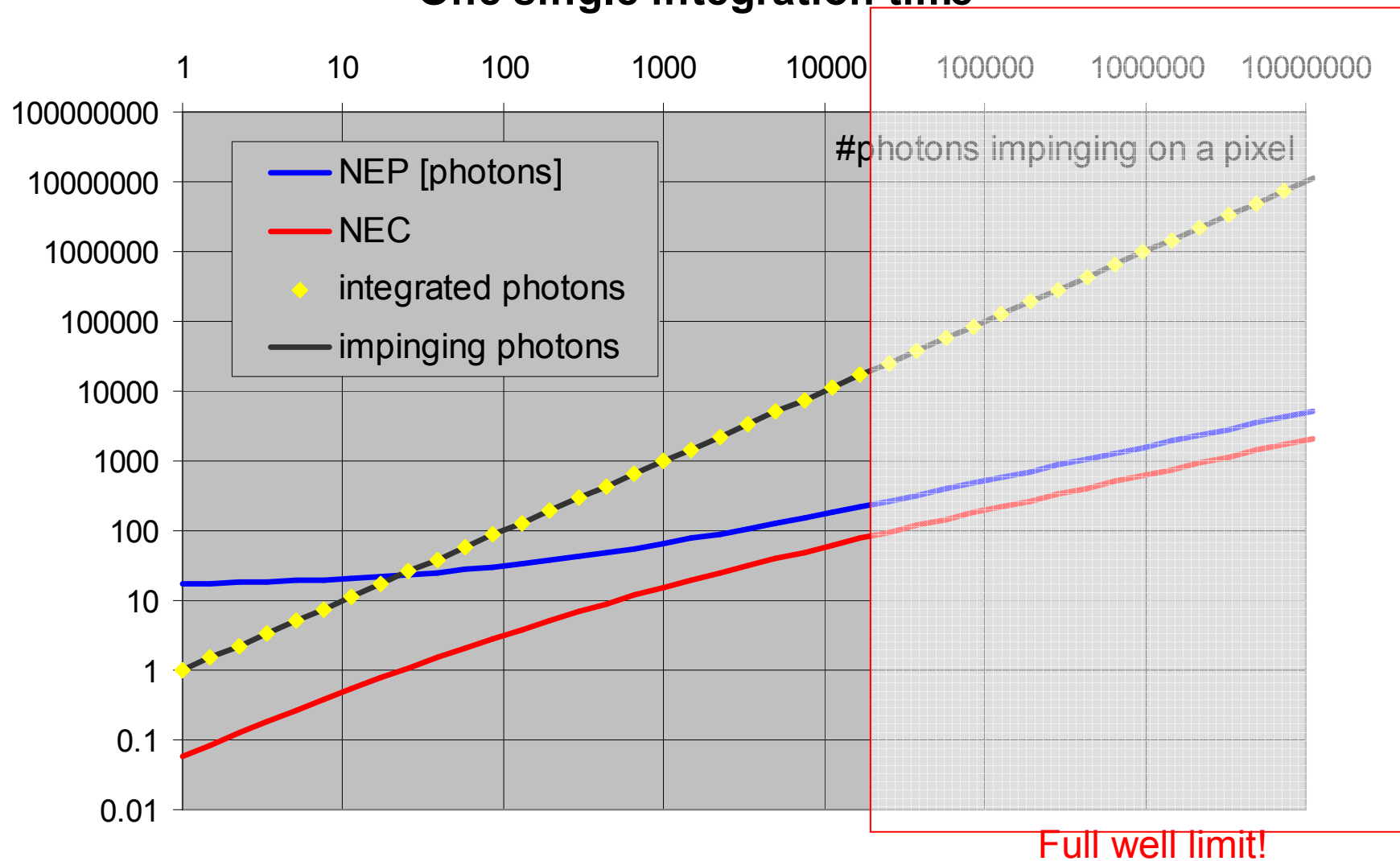
- QE = 40%
- $C_{\text{eff}} = 1\text{fF}$
- t_{int} = not specified

Full well limit \approx
 $1\text{fF} * 1\text{V} \approx 6000e^-$
15000 photons

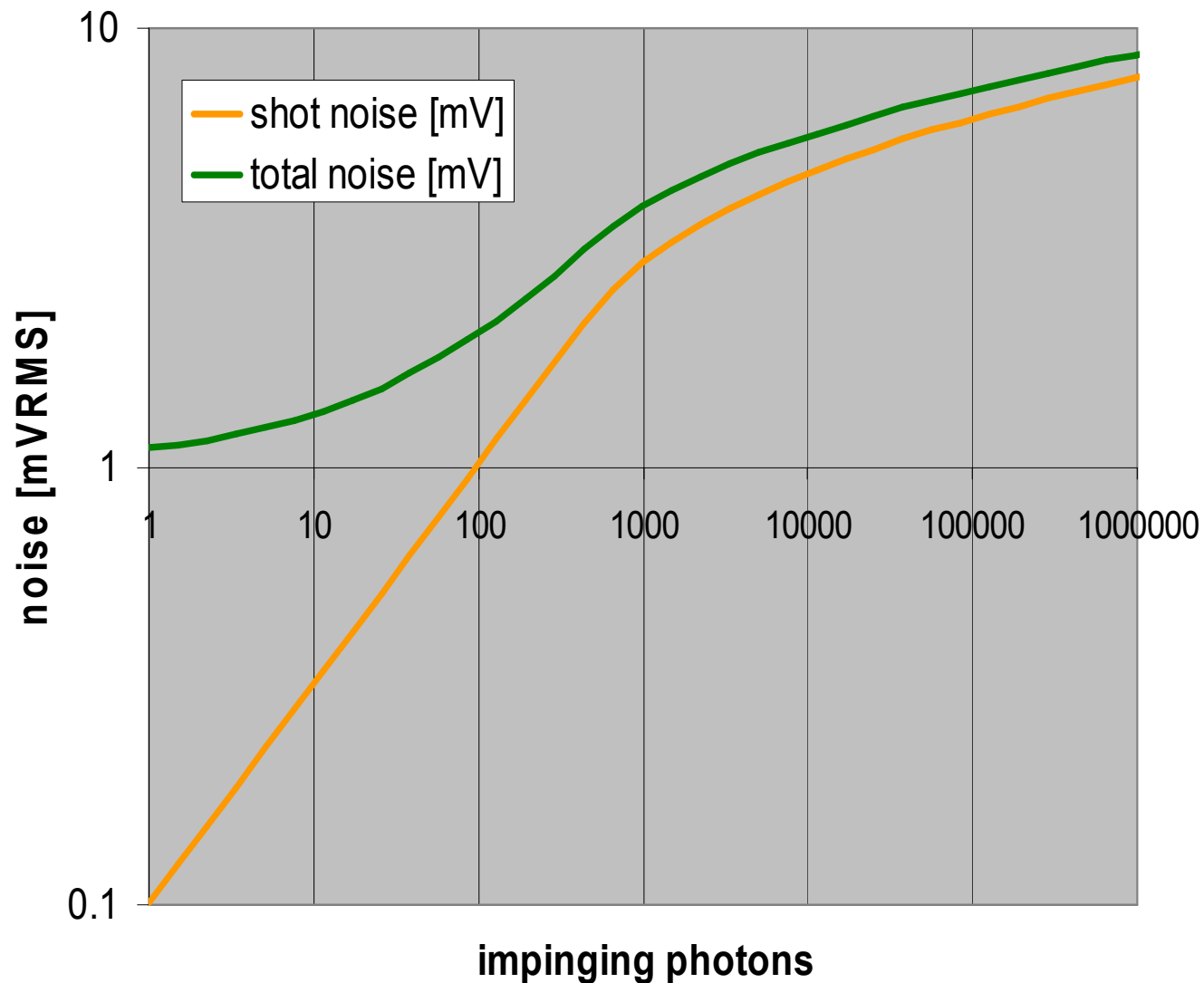


Linear response

One single integration time



Ideal response yielding $NEC \approx 10$



Noise sources

considered:

- PSN
- Read noise 1mV_{RMS}

QE = 40%

$C_{\text{eff}} = 1\text{fF}$

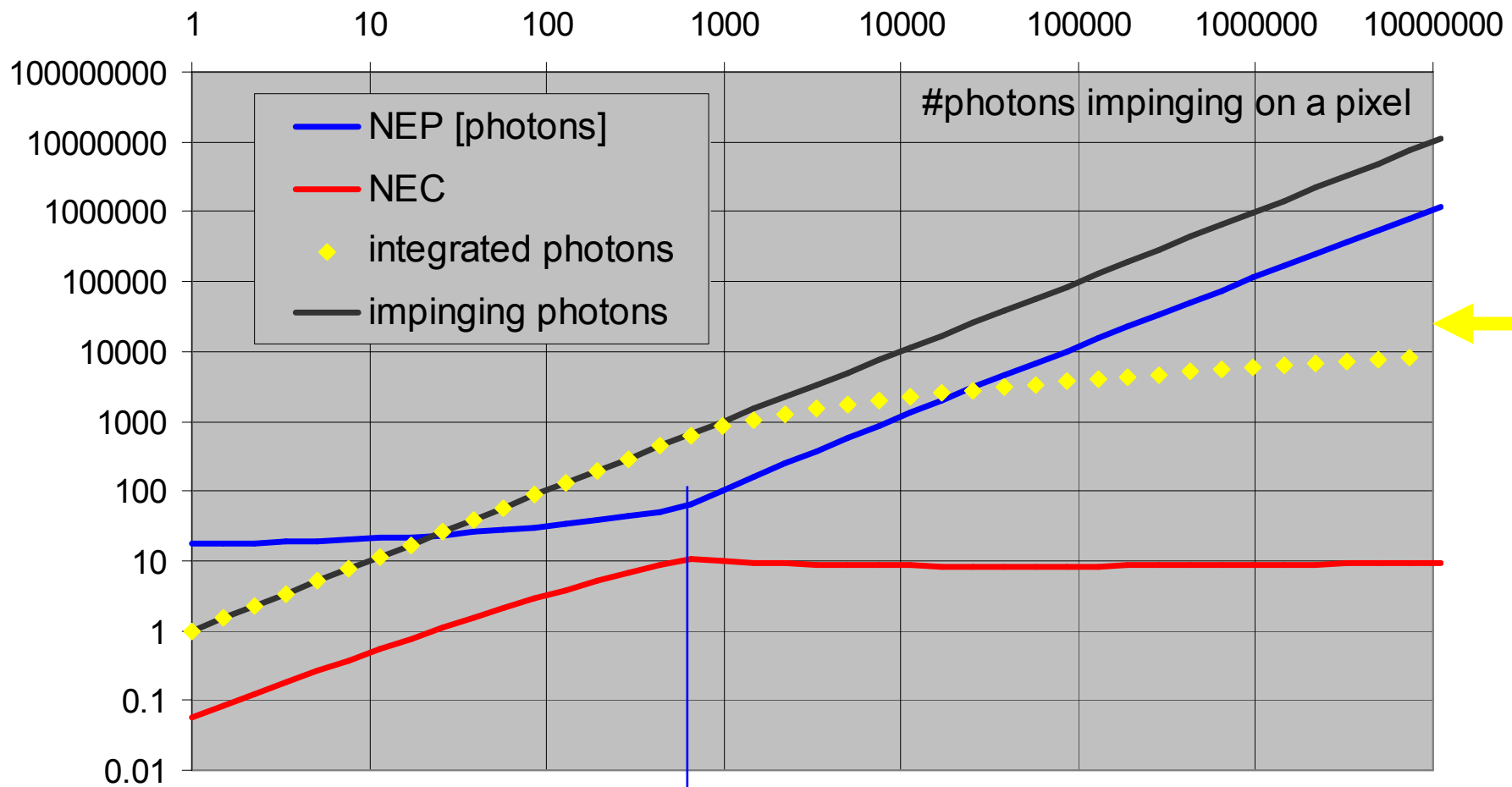
t_{int} = not specified

(Logarithmic)
response realized by
continuously reducing
the integration time
during the charge
acquisition, to have
 $NEC \approx 10$



Logarithmic response NEC \approx 10

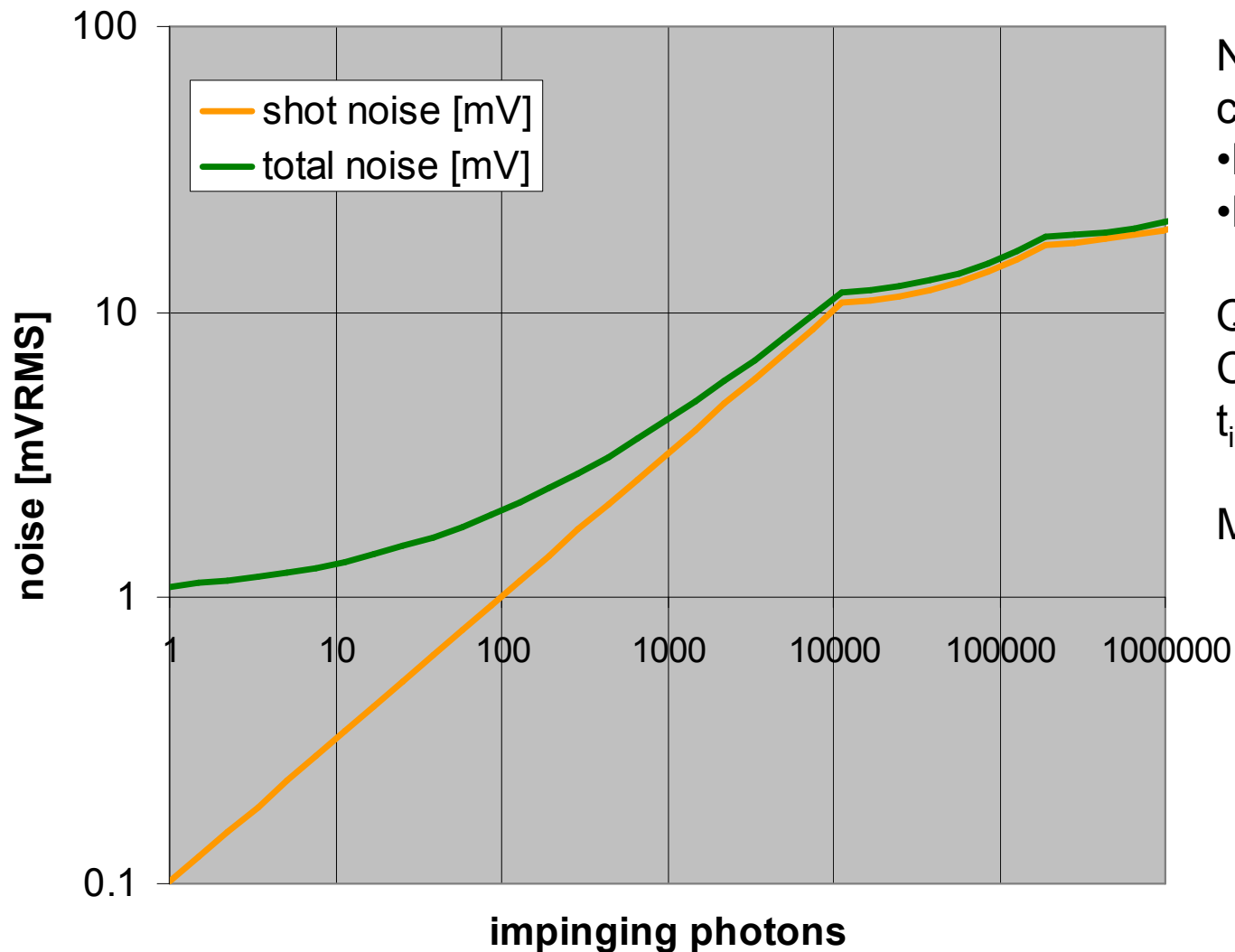
continuously varying integration time $t_{int}(Q)$



$t_{int} > t_{intmax} ?$ NEP is limited to linear case



Multiple slopes methods $NEC > 10$



Noise sources

considered:

- PSN
- Read noise 1mV_{RMS}

QE = 40%

$C_{\text{eff}} = 1\text{fF}$

t_{int} = not specified

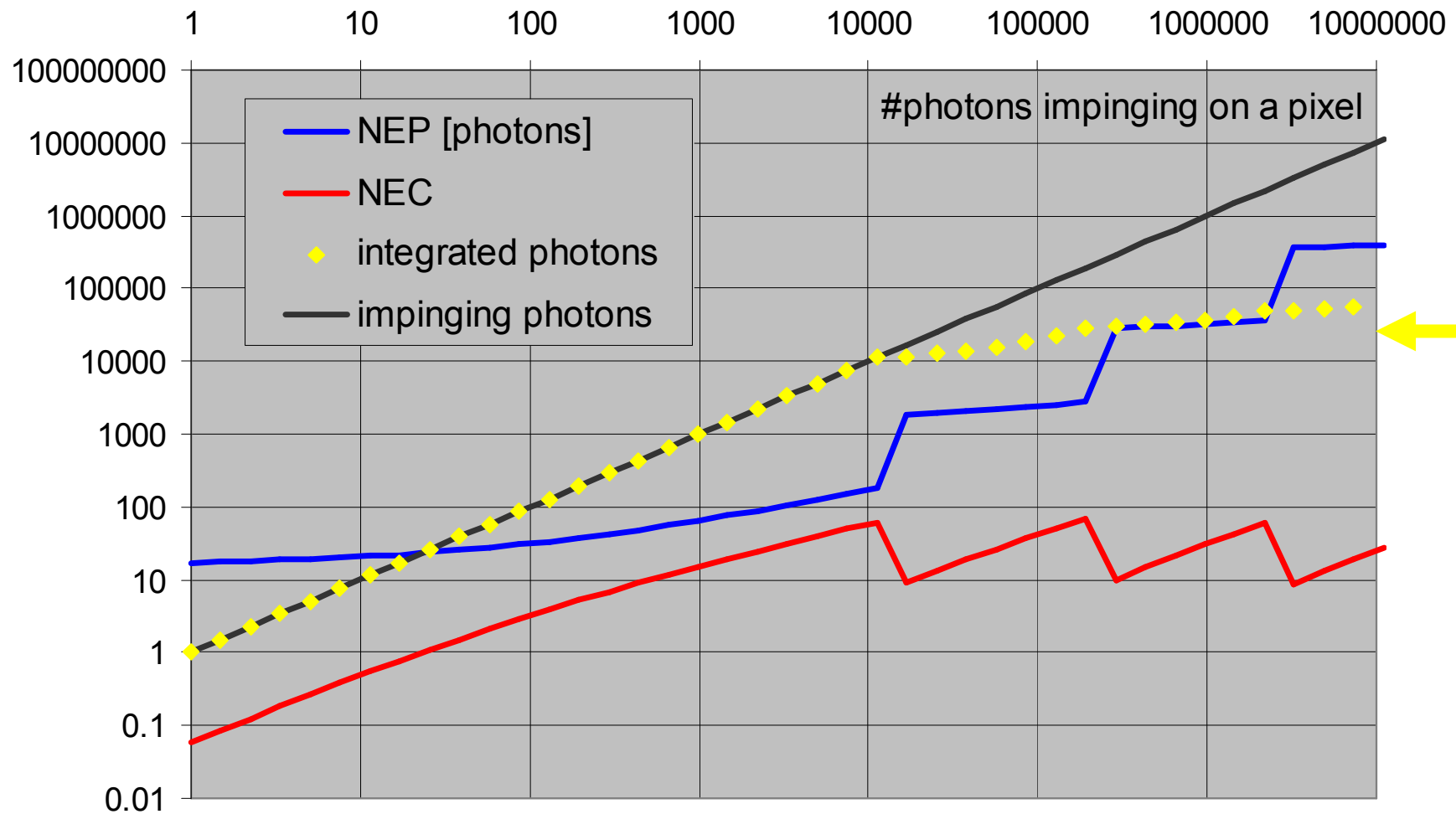
Multiple slopes

- 1st slope starts at 10000 photons (4000 electrons)
- Consecutive slopes have factor 10 lower integration time
- New slope starts only when $NEC \geq 10$ is assured



Multiple slopes methods $NEC > 10$

Multiple slopes using multiple integration times



Conclusions



Was there something you might want to remember?

- High (wide) dynamic range is a property of the scene. The sensor has to accommodate.
- How to accommodate: yielding a sufficient NEC in all parts of the image/scene
- The logarithmic response follows naturally when assuming a typical noise signature, and aiming for a constant, minimal NEC
- Piece-wise approximation (multiple slopes) of the ideal logarithmic response is not as good.
- How to implement? 😊 the next presentations



Thank you



Abbreviations and symbols

C_{eff}	charge to voltage transconductance
D	lens aperture
DCSN	dark current shot noise
DSNU	dark signal non uniformity
EMI	electro-magnetic interference
f	focal length
F	f-number $F=f/D$
FPN	fixed pattern noise
N	Noise, uncertainty on S
NEC	noise equivalent contrast [%]
NEP	noise equivalent power [W...]
P	optical power [W, photons/s, ...]
PR	photo response [V/W, V.m ² /W.s]
PRNU	PR non-uniformity

Q_{noise}	uncertainty on Q_{signal} [F, e ⁻]
Q_{photo}	(maximum) photo charge [F, e ⁻]
Q_{signal}	actual photo charge, due to electronic shutter
QE	quantum efficiency [electrons/photon]
RMS	root-mean-square, subscript denoting that the value is a distribution
S	Signal, normally equal to V_{signal}
SR	spectral response [A/W]
t_{int}	integration time, electronic shutter time
t_{intmax} time	maximum available integration time
V_{noise}	uncertainty on V_{signal} , = N

